

Blast Resistance of Unreinforced Masonary (URM) walls Retrofited with Nano-Reinforced Elastomeric Material

**M. Irshidat, Dr. A. Al-Ostaz,
Dr. A. Cheng, Dr. C. Mullen.**

University of Mississippi, Civil Engineering Department

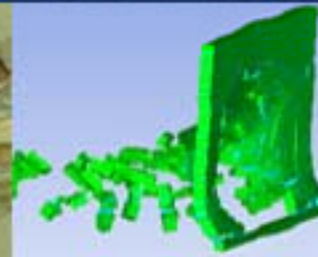
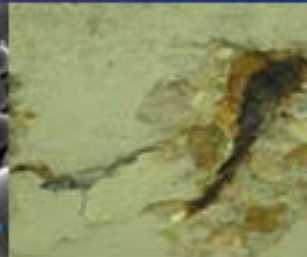
June 24-27-2009



From Quantum to Infrastructure



THE UNIVERSITY OF MISSISSIPPI



Outline

- Objectives
- Problem statement
- Experimental program
- Computational simulations
- Remarks/Conclusions

Objective

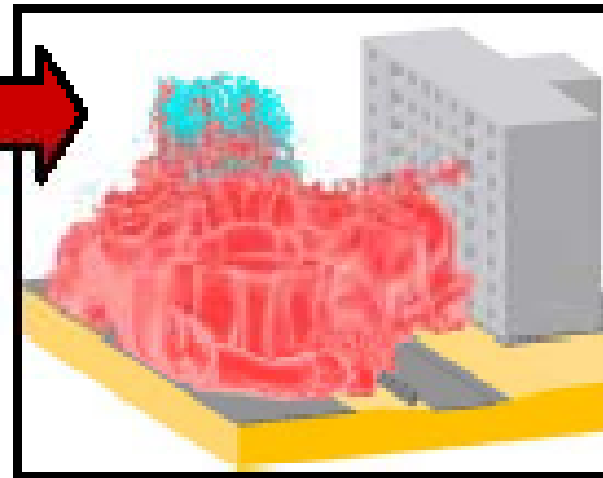
The main objective of this work is to investigate the viability of using Nano Particle Reinforced Elastomeric Materials (NPREM) to protect the masonry structures against blast loading experimentally and numerically.

Problem Statement

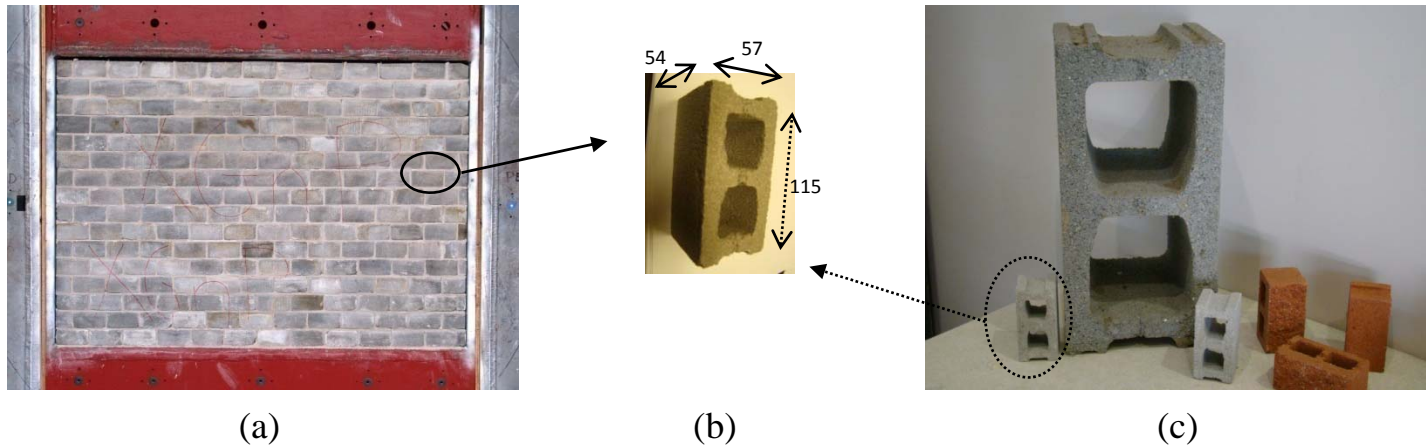


Full Scale Blast Test

**Numerical
Simulation**



Experimental Program



(a) Masonry wall dimensions (b) Concrete masonry unit brick (all dimensions in mm)
(c) comparison between full scale and scaled down dimensions of masonry unit

Three walls were tested at the US Army Engineer Research and Development Center (ERDC) using the blast simulator :

1. retrofitted with unreinforced polyurea
2. retrofitted with reinforced polyurea using exfoliated graphene nano platelets (XGnP)
3. retrofitted with reinforced polyurea using Polyhedral Oligomeric Silsesquioxane (POSS).

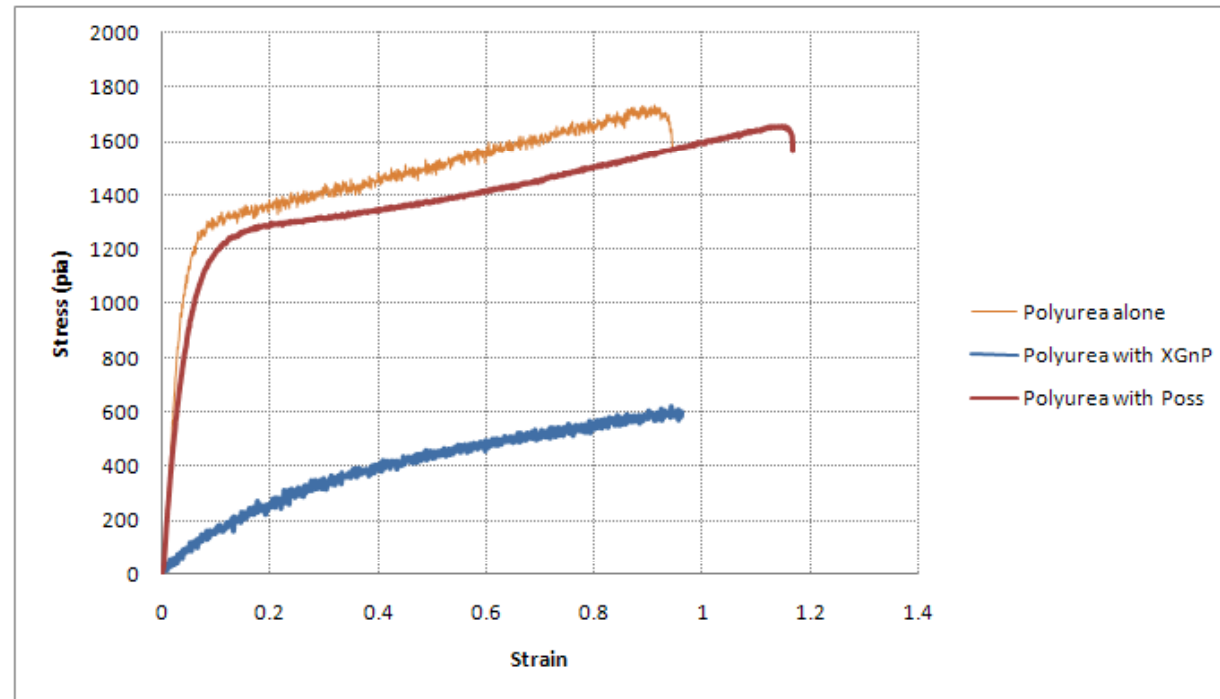
Retrofitting process



➤ Test Matrix of retrofit schemes

Wall Number	Retrofit Material
Wall #1	Polyurea alone
Wall #2	Polyurea reinforced with xGnP
Wall #3	Polyurea reinforced with POSS

➤ TYPICAL STRESS-STRAIN RELATION FOR RETROFITTED MATERIALS UNDER TENSILE LOADING



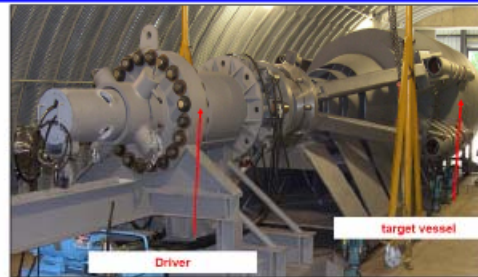
➤ RETROFITTED MATERIALS PROPERTIES

Material	Modulus of Elasticity (MPa/ psi)	Ultimate Strength (MPa/ psi)	Strain at Rupture (%)
Polyurea	229.689/ 33313.7	11.85/1718.3	95
Polyurea with xGnP	12.85/1863.4	4.48/649.8	96
Polyurea with POSS	199.80/28979	13.51/1958.7	113

Blast load testing

BLAST TEST FACILITY (ERDC - Vicksburg, MS)

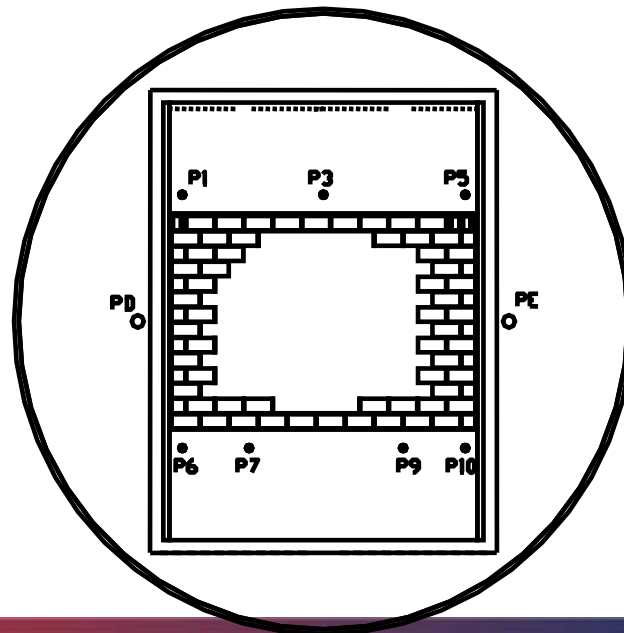
Blast Load Simulator (BLS)



The pressure loading is generated by releasing compressed air from the driver, the small (4") cylinder. Shock waves are generated at the front of the expanding compressed air as it travels toward the large diameter (17") end of the tube and strikes the test specimen mounted in the target vessel. The pressure loading at the target is a function of the driver pressure (up to 1500 psi), the driver volume, the length of the transition tube, and the venting used along the length of the tube. Waveforms created by the release of the compressed gases replicate the positive and negative loading phase associated with high-explosive yields up to 20,000 lb.

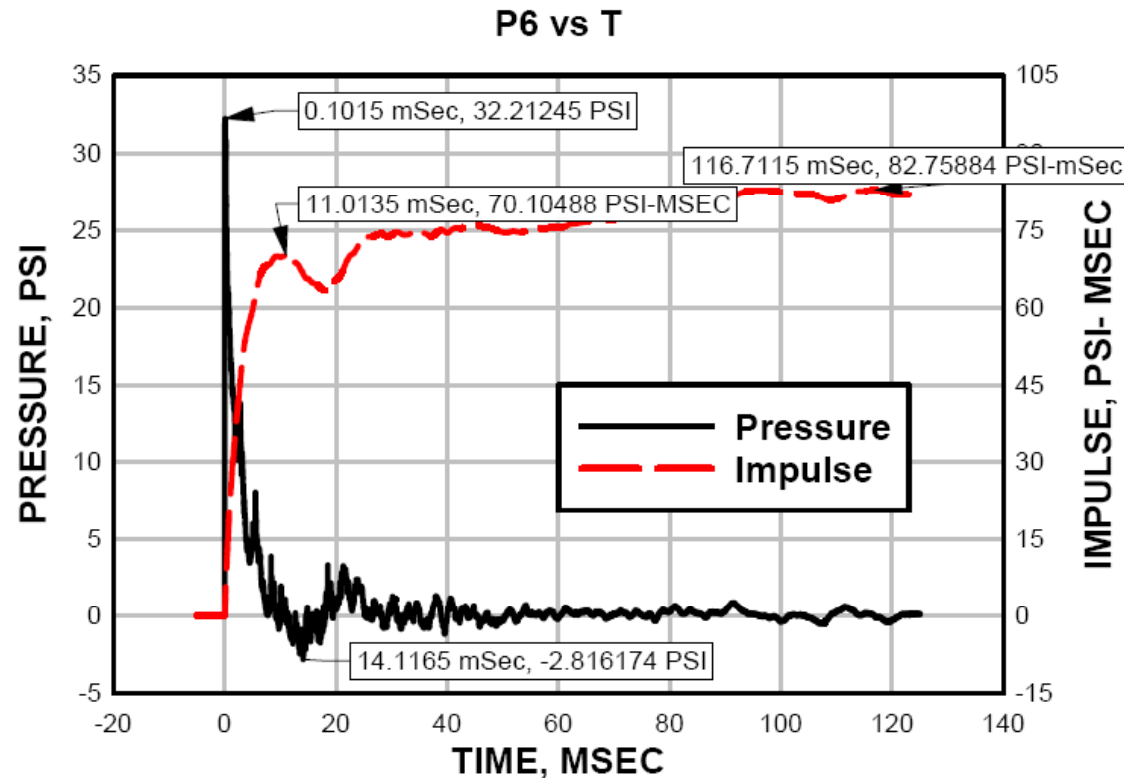


Geotechnical and Structures Laboratory



Gage	P	I
	(psi)	(psi-msec)
P1	33.65	71.7
P3	33.13	71.5
P5	29.5	72.1
P6	32.21	70.1
P7	31.63	71.5
P9	27.95	71.1
P10	30.87	71.6
PD	35.22	72.3
PE	31.6	73.2
Sum	285.76	645.1
Avg	31.75	71.7
IP1	0.37	

Typical pressure-time history and associated impulse time history obtained for Wall 3 using pressure Sensor.



Average values of reflected pressure and impulse for each wall

Wall Number	Pressure kPa, (psi)	Impulse (kPa.ms) (psi.ms)
Wall #1	208.22 (30.20)	366.80 (53.20)
Wall #2	224.91 (32.62)	496.42 (72.00)
Wall #3	218.91 (31.75)	494.35 (71.70)

➤ Experimental results



(a)



(b)



(c)

Wall #1 (a) Back View Before The Blast Event (b) Back View After The Blast Event
(c) Front View After The Blast Event



(a)



(b)



(c)

Wall #2 (a) Front View Before The Blast Event (b) Front View After The Blast Event
(c) Back View After The Blast Event

➤ Experimental results



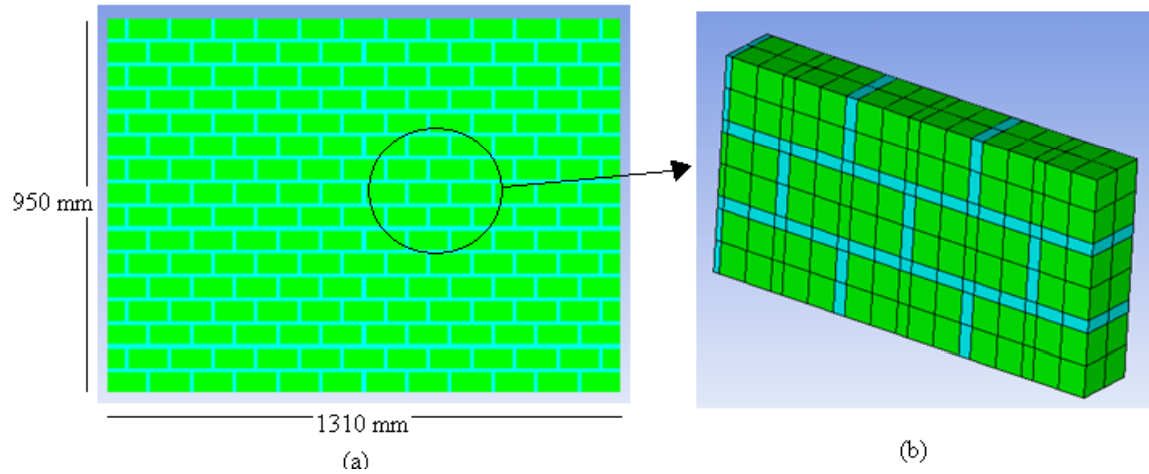
(a)



(b)

Wall #3 (a) back view after the blast event (b) front view after the blast event.

Computational simulations

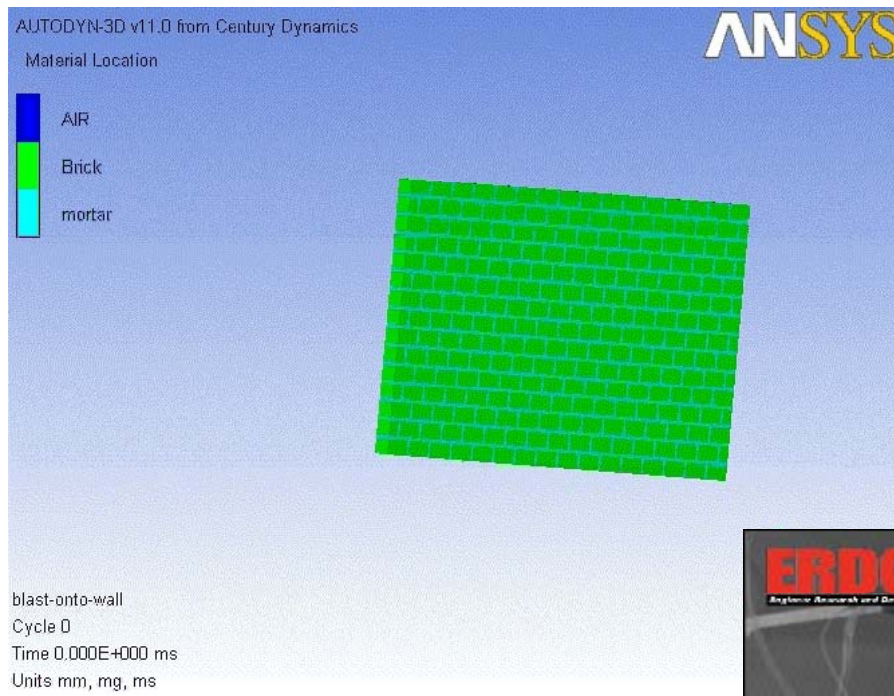


(a) Wall geometry (b) F.E. mesh

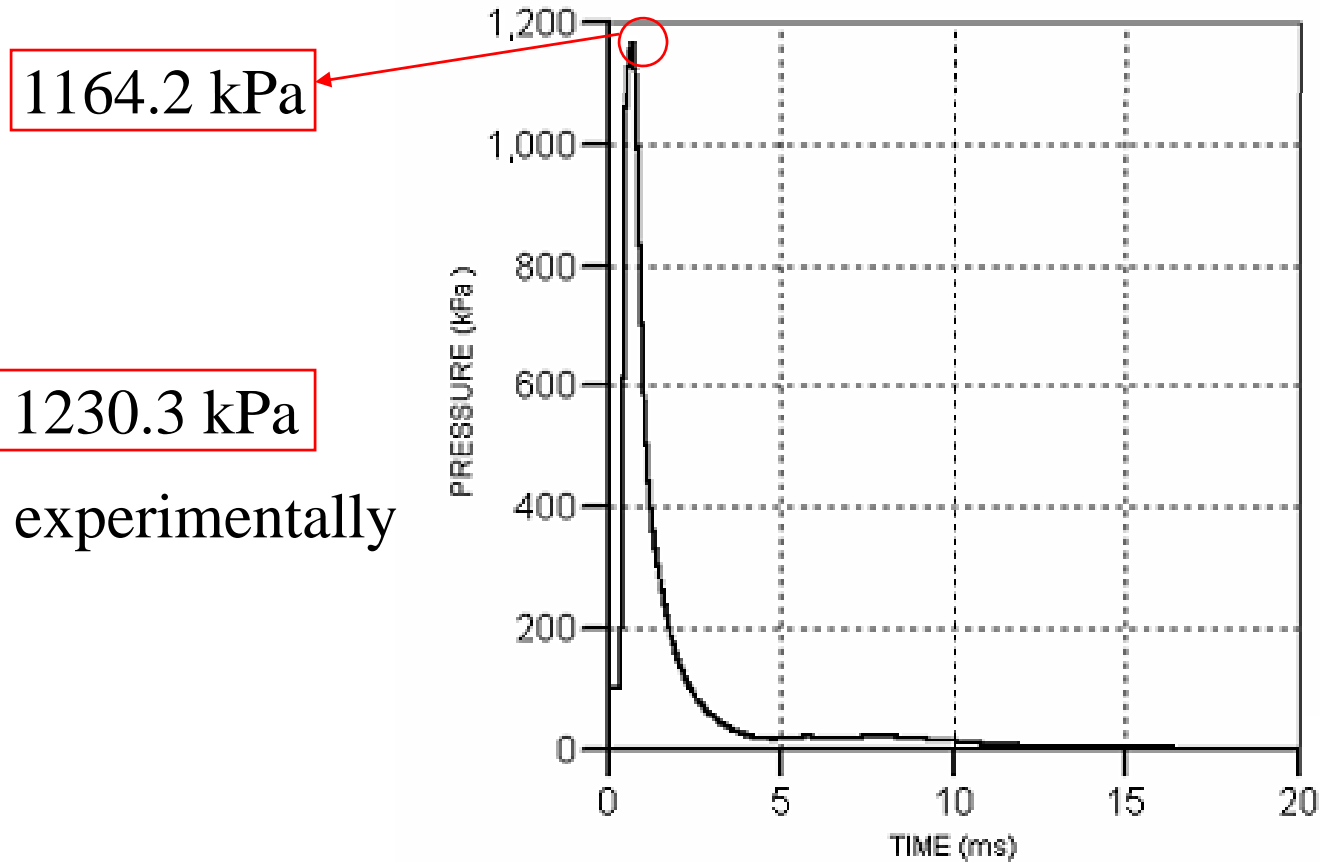
➤ Materials Models

Material	EOS	Strength Model	Failure Model
Masonry	Porous	Drucker-Prager	Hydrodynamic tensile failure (P_{min})
Mortar	Compaction	Mo Granular	Hydrodynamic tensile failure (P_{min})
Polyurea	Linear	Johnson-Cook	Principal Strain
Poyurea with POSS	Linear	Johnson-Cook	Principal Strain
Poyurea with xGnP	Linear	Johnson-Cook	Principal Strain

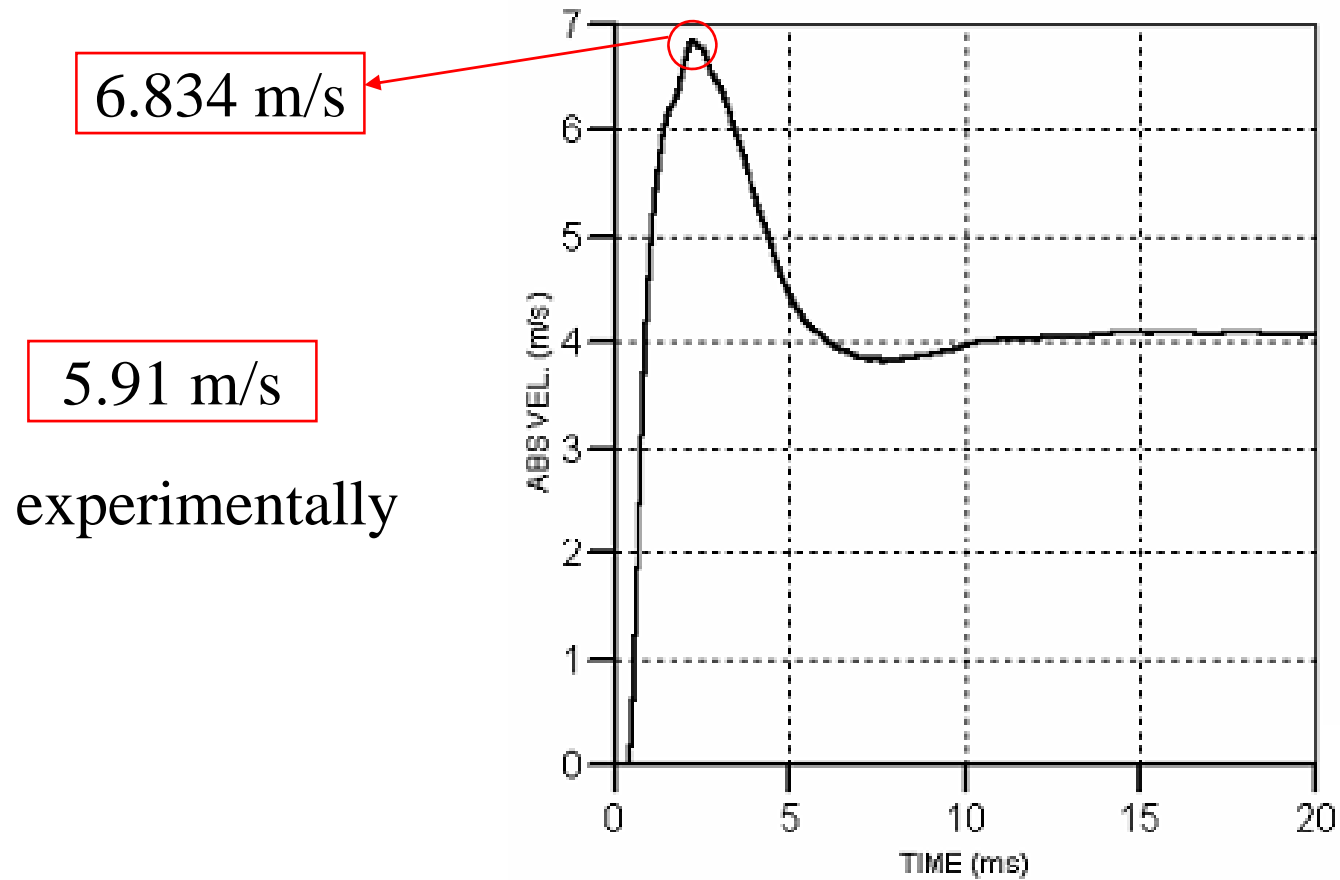
FE Model Validation (Un-Retrofitting Walls)



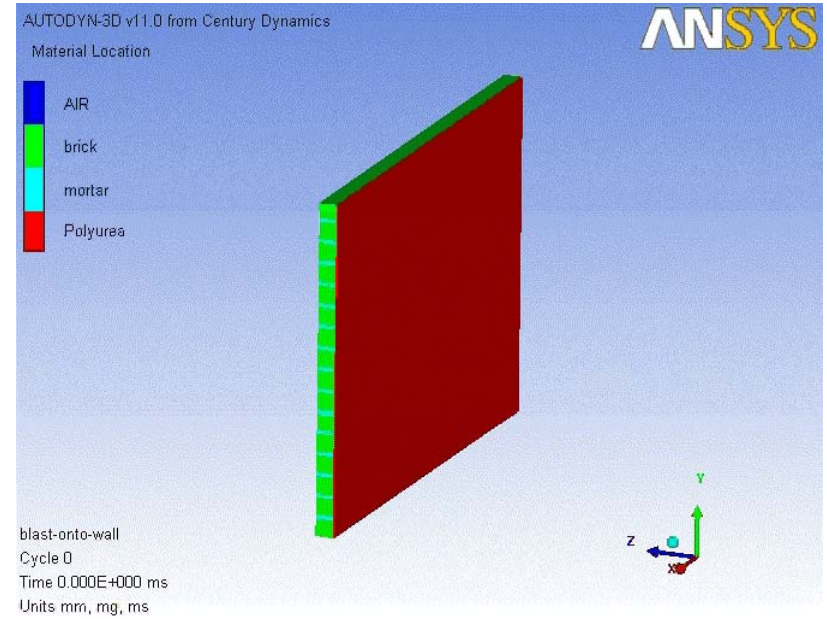
Pressure-Time history due to detonation just before the midpoint of the wall



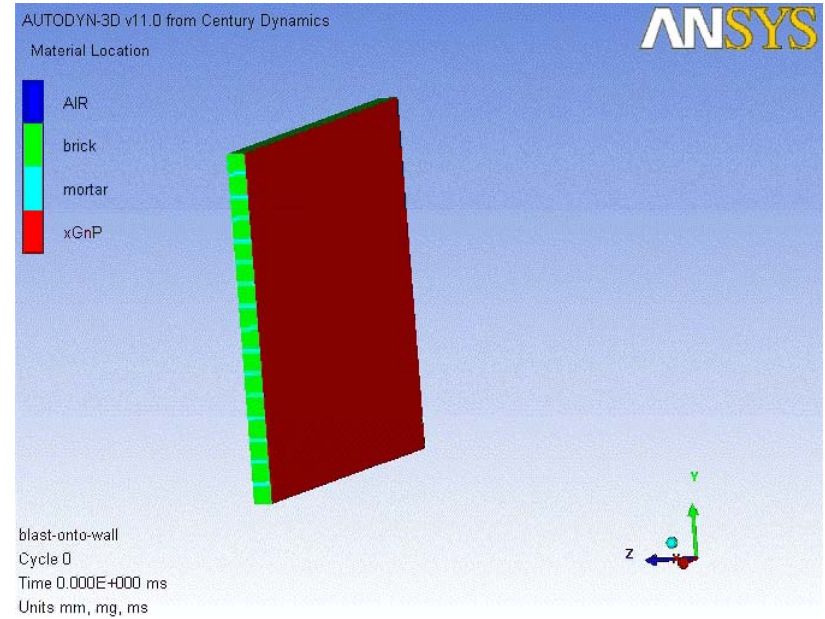
Debris velocity at midpoint of the wall



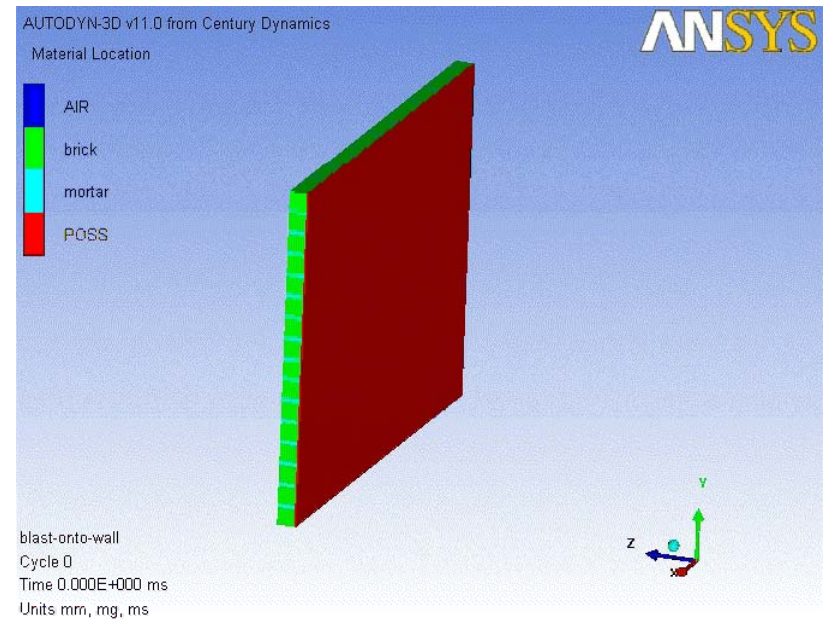
CMU wall retrofitted with unreinforced polyurea



CMU wall retrofitted with reinforced ployurea using xGnP



CMU wall retrofitted with reinforced ployurea using POSS



➤ Results comparison

Wall Number	Midpoint deflection at failure mm, (in.)		Maximum debris velocity m/s (in/ms)	
	experiment	FE simulation	experiment	FE simulation
Wall #1	91.4 (3.6)	96.27 (3.79)	3.86 (0.15)	5.21 (0.21)
Wall #2	76.4 (3.0)	113 (4.45)	7.47 (0.29)	6.144 (0.24)
Wall #3	120.65 (4.75)	112(4.41)	N.A	N.A

Remarks/Conclusions

- Results from blast experiments showed increase in ultimate flexural resistance achieved by both unreinforced and nano reinforced polyurea retrofit systems applied to URM.
- Whereas nano reinforcing polyurea with POSS nano material improved the performance of the elastomeric retrofit for blast loading, XGnP addition show very little improvement.
- It is important to develop physics-based models to better understand and engineer nano-structured materials for desired properties.

Acknowledgment

Funding received under a subcontract from the Department of Homeland Security-sponsored Southeast Region Research Initiative (SERRI) at the Department of Energy's Oak Ridge National Laboratory.

THANK YOU